



## Introduction

Most designers are familiar with oscillators (Pierce-Gate topology), but few really understand how they operate, let alone how to properly design an oscillator. In practice, most designers do not even really pay attention to the oscillator design until they realize the oscillator does not operate properly (usually when it is already being produced). This should not happen. Many systems or projects are delayed in their deployment because of a crystal not working as intended. The oscillator should receive its proper amount of attention during the design phase, well before the manufacturing phase. The designer would then avoid the nightmare scenario of products being returned.

This application note introduces the Pierce oscillator basics and provides some guidelines for a good oscillator design. It also shows how to determine the different external components and provides guidelines for a good PCB for the oscillator.

This document finally contains an easy guideline to select suitable crystals and external components, and it lists some recommended crystals (HSE and LSE) for STM32™ and STM8A/S microcontrollers in order to quick start development.

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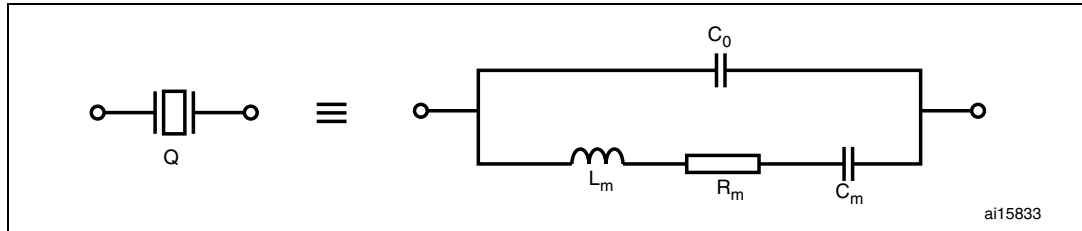
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# 1 Quartz crystal properties and model

A quartz crystal is a piezoelectric device transforming electric energy to mechanical energy and vice versa. The transformation occurs at the resonant frequency. The quartz crystal can be modeled as follows:

**Figure 1. Quartz crystal model**



$C_0$ : represents the shunt capacitance resulting from the capacitor formed by the electrodes

$L_m$ : (motional inductance) represents the vibrating mass of the crystal

$C_m$ : (motional capacitance) represents the elasticity of the crystal

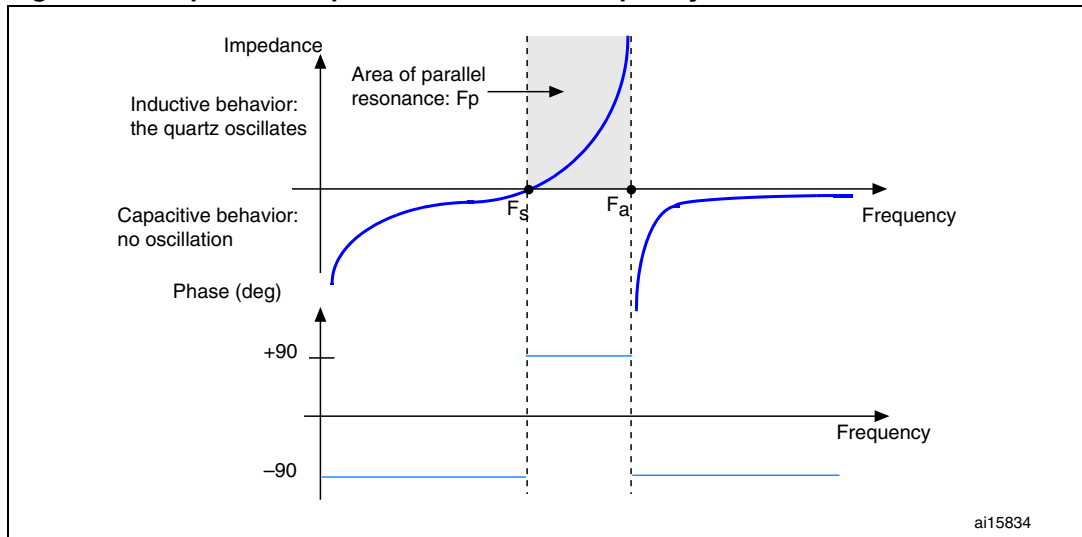
$R_m$ : (motional resistance) represents the circuit losses

The impedance of the crystal is given by the following equation (assuming that  $R_m$  is negligible):

$$Z = \frac{j}{\omega} \times \frac{\omega^2 L_m C_m - 1}{(C_0 + C_m) - \omega^2 L_m C_m C_0} \quad (1)$$

Figure 2 represents the impedance in the frequency domain.

**Figure 2. Impedance representation in the frequency domain**



$F_s$  is the series resonant frequency when the impedance  $Z = 0$ . Its expression can be deduced from equation (1) as follows:

$$F_s = \frac{1}{2\pi\sqrt{L_m C_m}} \quad (2)$$

$F_a$  is the anti-resonant frequency when impedance  $Z$  tends to infinity. Using equation (1), it is expressed as follows:

$$(3) \quad F_a = F_s \sqrt{1 + \frac{C_m}{C_0}}$$

The region delimited by  $F_s$  and  $F_a$  is usually called the area of parallel resonance (shaded area in [Figure 2](#)). In this region, the crystal operates in parallel resonance and behaves as an inductance that adds an additional phase equal to  $180^\circ$  in the loop. Its frequency  $F_p$  (or  $F_L$ : load frequency) has the following expression:

$$F_p = F_s \left( 1 + \frac{C_m}{2(C_0 + C_L)} \right) \quad (4)$$

From equation (4), it appears that the oscillation frequency of the crystal can be tuned by varying the load capacitor  $C_L$ . This is why in their datasheets, crystal manufacturers indicate the exact  $C_L$  required to make the crystal oscillate at the nominal frequency.

[Table 1](#) gives an example of equivalent crystal circuit component values to have a nominal frequency of 8 MHz.

**Table 1. Example of equivalent circuit parameters**

Equivalent component	Value
$R_m$	8 $\Omega$
$L_m$	14.7 mH
$C_m$	0.027 pF
$C_0$	5.57 pF

Using equations (2), (3) and (4) we can determine  $F_s$ ,  $F_a$  and  $F_p$  of this crystal:

$$F_s = 7988768 \text{ Hz} \text{ and } F_a = 8008102 \text{ Hz} .$$

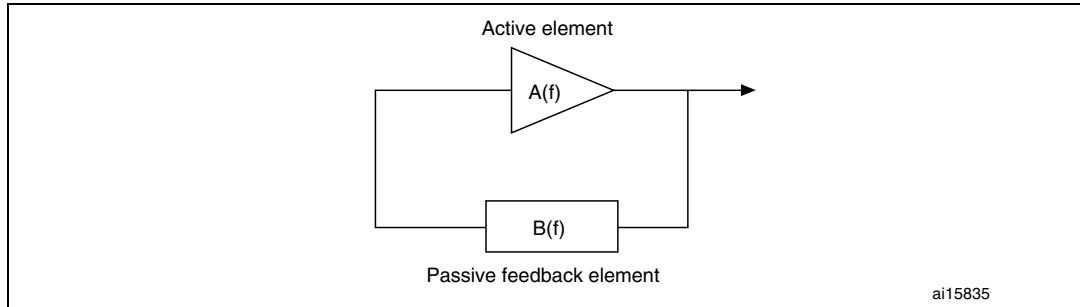
If the load capacitance  $C_L$  at the crystal electrodes is equal to 10 pF, the crystal will oscillate at the following frequency:  $F_p = 7995695 \text{ Hz} .$

To have an oscillation frequency of exactly 8 MHz,  $C_L$  should be equal to 4.02 pF.

## 2 Oscillator theory

An oscillator consists of an amplifier and a feedback network to provide frequency selection. [Figure 3](#) shows the block diagram of the basic principle.

**Figure 3. Oscillator principle**



Where:

- $A(f)$  is the complex transfer function of the amplifier that provides energy to keep the oscillator oscillating.

$$A(f) = |A(f)| \cdot e^{j\alpha(f)}$$

- $B(f)$  is the complex transfer function of the feedback that sets the oscillator frequency.

$$B(f) = |B(f)| \cdot e^{j\beta(f)}$$

To oscillate, the following Barkhausen conditions must be fulfilled. The closed-loop gain should be greater than 1 and the total phase shift of  $360^\circ$  is to be provided:

$$|A(f)| \cdot |B(f)| \geq 1 \text{ and } \alpha(f) + \beta(f) = 2\pi$$

The oscillator needs initial electric energy to start up. Power-up transients and noise can supply the needed energy. However, the energy level should be high enough to trigger oscillation at the required frequency. Mathematically, this is represented by  $|A(f)| \cdot |B(f)| \gg 1$ , which means that the open-loop gain should be much higher than 1. The time required for the oscillations to become steady depends on the open-loop gain.

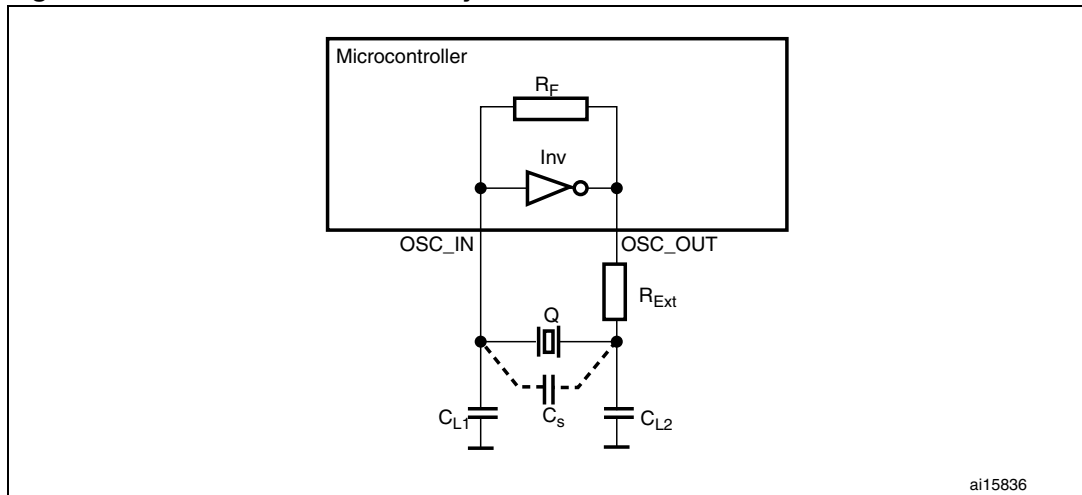
Meeting the oscillation conditions is not enough to explain why a crystal oscillator starts to oscillate. Under these conditions, the amplifier is very unstable, any disturbance introduced in this positive feedback loop system makes the amplifier unstable and causes oscillations to start. This may be due to power-on, a disable-to enable sequence, the thermal noise of the crystal, etc. It is also important to note that only noise within the range of serial-to parallel frequency can be amplified. This represents but a little amount of energy, which is why crystal oscillators are so long to start up.



### 3 Pierce oscillator

Pierce oscillators are commonly used in applications because of their low consumption, low cost and stability.

**Figure 4. Pierce oscillator circuitry**



Inv: the internal inverter that works as an amplifier

Q: crystal quartz or a ceramic resonator

$R_F$ : internal feedback resistor

$R_{Ext}$ : external resistor to limit the inverter output current

$C_{L1}$  and  $C_{L2}$ : are the two external load capacitors

$C_s$ : stray capacitance is the addition of the MCU pin capacitance (OSC\_IN and OSC\_OUT) and the PCB capacitance: it is a parasitical capacitance.

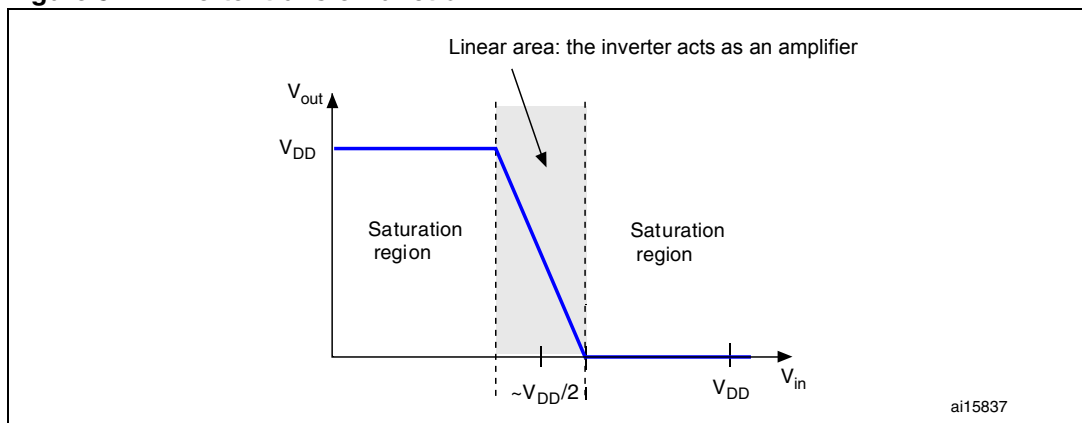
## 4 Pierce oscillator design

This section describes the different parameters and how to determine their values in order to be more conversant with the Pierce oscillator design.

### 4.1 Feedback resistor $R_F$

In most of the cases in ST microcontrollers,  $R_F$  is embedded in the oscillator circuitry. Its role is to make the inverter act as an amplifier. The feedback resistor is connected between  $V_{in}$  and  $V_{out}$  so as to bias the amplifier at  $V_{out} = V_{in}$  and force it to operate in the linear region (shaded area in [Figure 5](#)). The amplifier amplifies the noise (for example, the thermal noise of the crystal) within the range of serial to parallel frequency ( $F_a$ ,  $F_a$ ). This noise causes the oscillations to start up. In some cases, if  $R_F$  is removed after the oscillations have stabilized, the oscillator continues to operate normally.

**Figure 5. Inverter transfer function**



[Table 2](#) provides typical values of  $R_F$

**Table 2. Typical feedback resistor values for given frequencies**

Frequency	Feedback resistor range
32.768 kHz	10 to 25 M $\Omega$
1 MHz	5 to 10 M $\Omega$
10 MHz	1 to 5 M $\Omega$
20 MHz	470 k $\Omega$ to 5 M $\Omega$

## 4.2 Load capacitor $C_L$

The load capacitance is the terminal capacitance of the circuit connected to the crystal oscillator. This value is determined by the external capacitors  $C_{L1}$  and  $C_{L2}$  and the stray capacitance of the printed circuit board and connections ( $C_s$ ). The  $C_L$  value is specified by the crystal manufacturer. Mainly, for the frequency to be accurate, the oscillator circuit has to show the same load capacitance to the crystal as the one the crystal was adjusted for. Frequency stability mainly requires that the load capacitance be constant. The external capacitors  $C_{L1}$  and  $C_{L2}$  are used to tune the desired value of  $C_L$  to reach the value specified by the crystal manufacturer.

The following equation gives the expression of  $C_L$ :

$$C_L = \frac{C_{L1} \times C_{L2}}{C_{L1} + C_{L2}} + C_s$$

Example of  $C_{L1}$  and  $C_{L2}$  calculation:

For example if the  $C_L$  value of the crystal is equal to 15 pF and, assuming that  $C_s = 5$  pF, then:

$$C_L - C_s = \frac{C_{L1} \times C_{L2}}{C_{L1} + C_{L2}} = 10 \text{ pF}. \text{ That is: } C_{L1} = C_{L2} = 20 \text{ pF}.$$

## 4.3 Gain margin of the oscillator

The gain margin is the key parameter that determines whether the oscillator will start up or not. It has the following expression:

$$\text{gain}_{\text{margin}} = \frac{g_m}{g_{\text{mcrit}}}, \text{ where:}$$

- $g_m$  is the transconductance of the inverter (in mA/V for the high-frequency part or in  $\mu\text{A/V}$  for the low-frequency part: 32 kHz).
- $g_{\text{mcrit}}$  ( $g_m$  critical) depends on the crystal parameters.  
Assuming that  $C_{L1} = C_{L2}$ , and assuming that the crystal sees the same  $C_L$  on its pads as the value given by the crystal manufacturer,  $g_{\text{mcrit}}$  is expressed as follows:

$$g_{\text{mcrit}} = 4 \times \text{ESR} \times (2\pi F)^2 \times (C_0 + C_L)^2, \text{ where ESR} = \text{equivalent series resistor}$$

According to the Eric Vittoz theory: the impedance of the motional RLC equivalent circuit of a crystal is compensated by the impedance of the amplifier and the two external capacitances.

To satisfy this theory, the inverter transconductance ( $g_m$ ) must have a value  $g_m > g_{\text{mcrit}}$ . In this case, the oscillation condition is reached. A gain margin of 5 can be considered as a minimum to ensure an efficient startup of oscillations.

For example, to design the oscillator part of a microcontroller that has a  $g_m$  value equal to 25 mA/V, we choose a quartz crystal (from Fox) that has the following characteristics: frequency = 8 MHz,  $C_0 = 7$  pF,  $C_L = 10$  pF, ESR = 80  $\Omega$ . Will this crystal oscillate with this microcontroller?

Let us calculate  $g_{\text{mcrit}}$ :

$$g_{\text{mcrit}} = 4 \times 80 \times (2 \times \pi \times 8 \times 10^6)^2 \times (7 \times 10^{-12} + 10 \times 10^{-12})^2 = 0.23 \text{ mA/V}$$

Calculating the gain margin gives:

$$\text{gain}_{\text{margin}} = \frac{g_m}{g_{\text{m crit}}} = \frac{25}{0.23} = 107$$

The gain margin is very sufficient to start the oscillation and the “gain margin greater than 5” condition is reached. The crystal will oscillate normally.

If an insufficient gain margin is found (gain margin < 5) the oscillation condition is not reached and the crystal will not start up. You should then try to select a crystal with a lower ESR or/and with a lower  $C_L$ .

## 4.4 Drive level DL and external resistor $R_{\text{Ext}}$ calculation

The drive level and external resistor value are closely related. They will therefore be addressed in the same section.

### 4.4.1 Calculating drive level DL

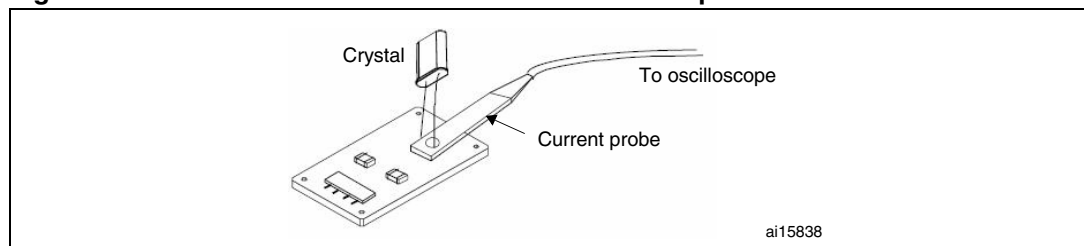
The drive level is the power dissipated in the crystal. It has to be limited otherwise the quartz crystal can fail due to excessive mechanical vibration. The maximum drive level is specified by the crystal manufacturer, usually in mW. Exceeding this maximum value may lead to the crystal being damaged.

The drive level is given by the following formula:  $DL = ESR \times I_Q^2$ , where:

- ESR is the equivalent series resistor (specified by the crystal manufacturer):  

$$ESR = R_m \times \left(1 + \frac{C_0}{C_L}\right)^2$$
- $I_Q$  is the current flowing through the crystal in RMS. This current can be displayed on an oscilloscope as a sine wave. The current value can be read as the peak-to-peak value ( $I_{PP}$ ). When using a current probe (as shown in [Figure 6](#)), the voltage scale of an oscilloscope may be converted into 1mA/1mV.

**Figure 6. Current drive measurement with a current probe**



So as described previously, when tuning the current with the potentiometer, the current through the crystal does not exceed  $I_{Qmax}$  RMS (assuming that the current through the crystal is sinusoidal).

Thus  $I_{Qmax}$  RMS is given by:

$$I_{Qmax} \text{RMS} = \sqrt{\frac{DL_{\text{max}}}{ESR}} = \frac{I_{Qmax} \text{PP}}{2\sqrt{2}}$$

Therefore the current through the crystal (peak-to-peak value read on the oscilloscope) should not exceed a maximum peak-to-peak current ( $I_{Q_{max}PP}$ ) equal to:

$$I_{Q_{max}PP} = 2 \times \sqrt{\frac{2 \times DL_{max}}{ESR}}$$

Hence the need for an external resistor ( $R_{Ext}$ ) (refer to [Section 4.4.3](#)) when  $I_Q$  exceeds  $I_{Q_{max}PP}$ . The addition of  $R_{Ext}$  then becomes mandatory and it is added to ESR in the expression of  $I_{Q_{max}}$ .

#### 4.4.2 Another drive level measurement method

The drive level can be computed as:

$DL = I_{QRMS}^2 \times ESR$ , where  $I_{QRMS}$  is the RMS AC current.

This current can be calculated by measuring the voltage swing at the amplifier input with a low-capacitance oscilloscope probe (no more than 1 pF). The amplifier input current is negligible with respect to the current through  $C_{L1}$ , so we can assume that the current through the crystal is equal to the current flowing through  $C_{L1}$ . Therefore the RMS voltage at this point is related to the RMS current by:

$I_{QRMS} = 2\pi F \times V_{RMS} \times C_{tot}$ , with:

- $F$  = crystal frequency
- $V_{RMS} = \frac{V_{pp}}{2\sqrt{2}}$ , where:  $V_{pp}$  is the voltage peak-to-peak measured at  $C_{L1}$  level
- $C_{tot} = C_{L1} + (C_s/2) + C_{probe}$  where:
  - $C_{L1}$  is the external load capacitor at the amplifier input
  - $C_s$  is the stray capacitance
  - $C_{probe}$  is the probe capacitance)

Therefore the drive level, DL, is given by:  $DL = \frac{ESR \times (\pi \times F \times C_{tot})^2 \times (V_{pp})^2}{2}$ .

This DL value must not exceed the drive level specified by the crystal manufacturer.

#### 4.4.3 Calculating external resistor $R_{Ext}$

The role of this resistor is to limit the drive level of the crystal. With  $C_{L2}$ , it forms a low-pass filter that forces the oscillator to start at the fundamental frequency and not at overtones (prevents the oscillator from vibrating at 3, 5, 7 etc. times the fundamental frequency). If the power dissipated in the crystal is higher than the value specified by the crystal manufacturer, the external resistor  $R_{Ext}$  becomes mandatory to avoid overdriving the crystal. If the power dissipated in the selected quartz is less than the drive level specified by the crystal manufacturer, the insertion of  $R_{Ext}$  is not recommended and its value is then 0  $\Omega$ .

An initial estimation of  $R_{Ext}$  is obtained by considering the voltage divider formed by  $R_{Ext}/C_{L2}$ . Thus, the value of  $R_{Ext}$  is equal to the reactance of  $C_{L2}$ .

Therefore:  $R_{Ext} = \frac{1}{2\pi FC_2}$ .

Let us put:

- oscillation frequency  $F = 8$  MHz
- $C_{L2} = 15$  pF

Then:  $R_{Ext} = 1326 \Omega$

The recommended way of optimizing  $R_{Ext}$  is to first choose  $C_{L1}$  and  $C_{L2}$  as explained earlier and to connect a potentiometer in the place of  $R_{Ext}$ . The potentiometer should be initially set to be approximately equal to the capacitive reactance of  $C_{L2}$ . It should then be adjusted as required until an acceptable output and crystal drive level are obtained.

**Caution:** After calculating  $R_{Ext}$  it is recommended to recalculate the gain margin (refer to [Section 4.3: Gain margin of the oscillator](#)) to make sure that the addition of  $R_{Ext}$  has no effect on the oscillation condition. That is, the value of  $R_{Ext}$  has to be added to ESR in the expression of  $g_{m_{crit}}$  and  $g_m \gg g_{m_{crit}}$  must also remain true:

$$g_m \gg g_{m_{crit}} = 4 \times (ESR + R_{Ext}) \times (2 \times \pi \times F)^2 \times (C_0 + C_L)^2$$

**Note:** If  $R_{Ext}$  is too low, there is no power dissipation in the crystal. If  $R_{Ext}$  is too high, there is no oscillation: the oscillation condition is not reached.

## 4.5 Startup time

It is the time that take the oscillations to start and become stable. This time is longer for a quartz than for a ceramic resonator. It depends on the external components:  $C_{L1}$  and  $C_{L2}$ . The startup time also depends on the crystal frequency and decreases as the frequency rises. It also depends on the type of crystal used: quartz or ceramic resonator (the startup time for a quartz is very long compared to that of a ceramic resonator). Startup problems are usually due to the gain margin (as explained previously) linked to  $C_{L1}$  and  $C_{L2}$  being too small or too large, or to ESR being too high.

The startup times of crystals for frequencies in the MHz range are within the ms range.

The startup time of a 32 kHz crystal is within the 1 s to 5 s range.

## 4.6 Crystal pullability

Pullability refers to the change in frequency of a crystal in the area of usual parallel resonance. It is also a measure of its frequency change for a given change in load capacitance. A decrease in load capacitance causes an increase in frequency. Conversely, an increase in load capacitance causes a decrease in frequency. Pullability is given by the following formula:

$$\text{Pullability}_{(\text{PPM}/\text{pF})} = \frac{C_m \times 10^6}{2 \times (C_0 + C_L)^2}$$

## 5 Easy guideline for the selection of suitable crystal and external components

This section gives a recommended procedure to select suitable crystal/external components. The whole procedure is divided into three main steps:

### Step1: Calculate the gain margin

(please refer to [Section 4.3: Gain margin of the oscillator](#))

- Choose a crystal and go to the references (chosen crystal + microcontroller datasheets)
- Calculate the oscillator gain margin and check if it greater than 5:  
If Gain margin < 5, the crystal is not suitable, choose another with a lower ESR or/and a lower  $C_L$ . Redo step 1.  
If Gain margin > 5, go to step 2.

### Step2: Calculate the external load capacitors

(please refer to [Section 4.2: Load capacitor CL](#))

Calculate  $C_{L1}$  and  $C_{L2}$  and check if they match the exact capacitor value on market or not:

- If you found the exact capacitor value then the oscillator will oscillate at the exact expected frequency. You can proceed to step 3.
- If you did not find the exact value and:
  - frequency accuracy is a key issue for you, you can use a variable capacitor to obtain the exact value. Then you can proceed to step 3.
  - frequency accuracy is not critical for you, choose the nearest value found on market and go to step 3.

### Step3: Calculate the drive level and external resistor

(please refer to [Section 4.4: Drive level DL and external resistor RExt calculation](#))

- Compute DL and check if is greater or lower than  $DL_{crystal}$ :
  - If  $DL < DL_{crystal}$ , no need for an external resistor. Congratulations you have found a suitable crystal.
  - If  $DL > DL_{crystal}$ , you should calculate  $R_{Ext}$  in order to have:  $DL < DL_{crystal}$ . You should then recalculate the gain margin taking  $R_{Ext}$  into account. If you find that gain margin > 5, congratulations, you have found a suitable crystal. If not, then this crystal will not work and you have to choose another. Return to step 1 to run the procedure for the new crystal.

## 6 Some recommended crystals for STM32™ microcontrollers

### 6.1 HSE part

#### 6.1.1 Part numbers of recommended 8 MHz crystals

**Table 3. EPSON®**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
MA-406 or MA-505 or MA-506 (8 MHz)	80 Ω	10 pF	5 pF	137.4	SMD

**Table 4. HOSONIC ELECTRONIC**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
HC-49S-8 MHz	80 Ω	10 pF	7 pF	107	Through-hole

**Table 5. CTS®**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
ATS08A	60 Ω	20 pF	7 pF	56.9	Through-hole
ATS08ASM	60 Ω	20 pF	7 pF	56.9	SMD

**Table 6. FOXElectronics®**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
FOXSLF/080-20	80 Ω	20 pF	7 pF	43.1	Through-hole
FOXSDLF/080-20	80 Ω	20 pF	7 pF	43.1	SMD
PFXLF/080-20	80 Ω	20 pF	7 pF	43.1	SMD

#### 6.1.2 Part numbers of recommended 8 MHz ceramic resonators

[Table 7](#) and [Table 8](#) give the references of recommended CERALOCK® ceramic resonator for the STM32™ microcontrollers provided and certified by Murata.

**Table 7. Recommendable condition (for consumer)**

Part number	C <sub>L</sub>	Package
CSTCE8M00G55-R0	Embedded load capacitors C <sub>L1</sub> = C <sub>L2</sub> = 33 pF	SMD

**Table 8. Recommendable condition (for CAN bus)**

Part number	C <sub>L</sub>	Package
CSTCE8M00G15C**-R0 <sup>(1)</sup>	Embedded load capacitors C <sub>L1</sub> = C <sub>L2</sub> = 33 pF	SMD

1. Refer to the datasheet of the resonator for details on the two asterisks.



For other Murata resonators recommended for STM32 microcontrollers, please refer to the following link:

<http://search.murata.co.jp/Ceramy/ICListAction.do?sKeyHin=STM32&sKeyMak=ST-MICROELECTRONICS&sLang=en&sParam=STM32>

### 6.1.3 Part numbers of recommended 25 MHz crystals (Ethernet applications)

**Table 9. HOSONIC ELECTRONIC**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
6FA25000F10M11	40 Ω	10pF	7pF	21.91	SMD
SA25000F10M11	40 Ω	10pF	7pF	21.91	Through-hole

**Table 10. FOXElectronics®**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
FOXSLF/250F-20	30 Ω	20 pF	7 pF	11.58	Through-hole
FOXSDLF/250F-20	30 Ω	20 pF	7 pF	11.58	SMD
PFXLF250F-20	30 Ω	20 pF	7 pF	11.58	SMD

**Table 11. CTS®**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
ATS25A	30 Ω	20 pF	7 pF	11.58	Through-hole
ATS25ASM	30 Ω	20 pF	7 pF	11.58	SMD

### 6.1.4 Part numbers of recommended 14.7456 MHz crystals (audio applications)

**Table 12. FOXElectronics®**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
FOXSLF/147-20	40 Ω	20 pF	7 pF	24.97	Through-hole
FOXSDLF/147-20	40 Ω	20 pF	7 pF	24.97	SMD

**Table 13. ABRACON™**

Part number	ESR	C <sub>L</sub>	C <sub>0</sub>	Gain margin	Package
ABMM2-14.7456 MHz	50 Ω	18 pF	7 pF	29.3	SMD

## 6.2 LSE part

For the LSE part of STM32™ microcontrollers, it is recommended to use a crystal with  $C_L < 7$  pF.

**Table 14. EPSON TOYOCOM**

Part number	ESR	$C_L$	$C_0$	Gain margin	Package
C-2-Type	35 kΩ	6 pF	2 pF	13.5	Through-hole
C-4-Type	55 kΩ	6 pF	2 pF	8.5	Through-hole

**Table 15. JFVNY®**

Part number	ESR	$C_L$	$C_0$	Gain margin	Package
DT-38G06	30 kΩ	6 pF	1.3 pF	18.44	Through-hole
MC306G06	50 kΩ	6 pF	2 pF	9.3	SMD

**Table 16. KDS**

Part number	ESR	$C_L$	$C_0$	Gain margin	Package
SM-26F	80 kΩ	6 pF	1.1 pF	7.3	Through-hole

## 7 Some recommended crystals for STM8A/S microcontrollers

### 7.1 Part numbers of recommended crystal oscillators

Table 17. KYOCERA

Part number	Freq.	ESR	CL	Drive level (DL)
CX5032GA08000H0QSWZZ	8 MHz	300 $\Omega$ max	12 pF	500 $\mu$ W max
CX5032GA16000H0QSWZZ	16 MHz	100 $\Omega$ max	12 pF	300 $\mu$ W max
CX8045GA08000H0QSWZZ	8 MHz	200 $\Omega$ max	12 pF	500 $\mu$ W max
CX8045GA16000H0QSWZZ	16 MHz	50 $\Omega$ max	12 pF	300 $\mu$ W max

### 7.2 Part numbers of recommended ceramic resonators

[Table 18](#) and [Table 19](#) give the references of recommended CERALOCK® ceramic resonators for the STM8A microcontrollers provided and certified by Murata.

Table 18. Recommendable conditions (for consumer)

Part number	Freq.	CL
CSTCR4M00G55B-R0	4 MHz	$C_{L1} = C_{L2} = 39$ pF
CSTCE8M00G55A-R0	8 MHz	$C_{L1} = C_{L2} = 33$ pF
CSTCE16M0G55A-R0	16 MHz	$C_{L1} = C_{L2} = 15$ pF

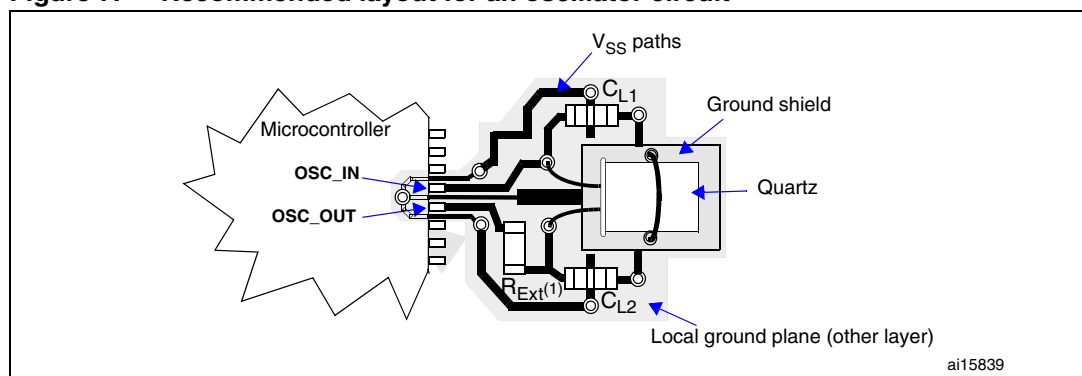
Table 19. Recommendable conditions (for CAN-BUS)

Part number	Freq.	CL
CSTCR4M00G15C**-R0	4 MHz	$C_{L1} = C_{L2} = 39$ pF
CSTCR8M00G15C**-R0	8 MHz	$C_{L1} = C_{L2} = 33$ pF
CSTCE16M0V13C**-R0	16 MHz	$C_{L1} = C_{L2} = 15$ pF

## 8 Some PCB hints

1. High values of stray capacitance and inductances must be avoided as much as possible as they might give rise to an undesired mode of oscillation and lead to startup problems.  
In addition, high-frequency signals should be avoided near the oscillator circuitry.
2. Reduce trace lengths as much as possible.
3. Use ground planes to isolate signals and reduce noise. For instance, the use of a local ground plane on the PCB layer immediately below the crystal guard ring is a good solution to isolate the crystal from undesired coupling with signals on other PCB layers (crosstalk). Note that the ground plane is needed in the vicinity of the crystal only and not on the entire board (see [Figure 7](#)).
4. The  $V_{SS}$  paths can also be routed as shown in [Figure 7](#). In this way, the  $V_{SS}$  paths isolate the oscillator input from the output and the oscillator from adjacent circuitry. The unterminated  $V_{SS}$  paths that end under  $C_{L1}$  and  $C_{L2}$  are not in contact with the ground shield under the quartz. All  $V_{SS}$  vias in [Figure 7](#) are connected to the local ground plane (except for the quartz pads).
5. Use decoupling capacitors between each  $V_{DD}$  path and the closest  $V_{SS}$  path to reduce noise.

**Figure 7. Recommended layout for an oscillator circuit**



**Note:**  $R_{Ext}$  is mandatory only if the dissipated power in the crystal exceeds the drive level specified by the crystal manufacturer. Otherwise, its value is  $0 \Omega$  (refer to [Section 4.4: Drive level DL and external resistor RExt calculation](#) for more details).

## 9 Conclusion

The most important parameter is the gain margin of the oscillator, which determines if the oscillator will start up or not. This parameter has to be calculated at the beginning of the design phase to choose the suitable crystal for the application. The second parameter is the value of the external load capacitors that have to be selected in accordance with the  $C_L$  specification of the crystal (provided by the crystal manufacturer). This determines the frequency accuracy of the crystal. The third parameter is the value of the external resistor that is used to limit the drive level. In the 32 kHz oscillator part, however, it is not recommended to use an external resistor.

Because of the number of variables involved, in the experimentation phase you should use components that have exactly the same properties as those that will be used in production. Likewise, you should work with the same oscillator layout and in the same environment to avoid unexpected behavior and therefore save time.

## 10 Revision history

**Table 20. Document revision history**

Date	Revision	Changes
20-Jan-2009	1	Initial release.
10-Nov-2009	2	DL formula corrected in <a href="#">Section 4.4.2: Another drive level measurement method</a> . Package column added to all tables in <a href="#">Section 6: Some recommended crystals for STM32™ microcontrollers</a> . Recommended part numbers updated in <a href="#">Section 6.1: HSE part</a> and <a href="#">Section 6.2: LSE part</a> . <a href="#">Section 6.1.3: Part numbers of recommended 25 MHz crystals (Ethernet applications)</a> added. <a href="#">Section 6.1.4: Part numbers of recommended 14.7456 MHz crystals (audio applications)</a> added.
27-Apr-2010	3	Added <a href="#">Section 7: Some recommended crystals for STM8A/S microcontrollers</a> .

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